

An Experimental Approach for Balancing a Vibratory System Considering Vibrational Characteristics

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Abstract

This paper presents the condition monitoring in terms of vibration of a static and dynamic balancing vibratory system which comprises a sturdy base unit, four flexible mounts, a steel shaft, low friction horizontal bearing, a set of four rotating masses where each masses contains a various circular insert. As for the rotating shaft, a signature of vibration has been identified due to mass imbalance which can be balanced by static or dynamic. For balancing the rotating mass system, the angular and longitudinal position of the 4th mass is settled to a perfect position for which fewer amount of vibration obtained in the base along with the vertical stands. A CSI 2140 machinery condition analyzer enumerates the vibrational data obtained at different angular spaces of the 4th mass at the rotating shaft and afterward, acquired data is compared with the ISO standard chart to identify the condition of the apparatus. It has been experienced that when the 4th mass is at an angular position of 338° in clockwise direction, the apparatus is in the perfect balanced position and the amplitude of vibration which has overall RMS value of 0.74770mm/s at accelerometer input A, 5.29330 mm/s at accelerometer input B and 1.32002 mm/s at accelerometer input C comparatively lower than any other angular position of the mass. Moreover, this paper includes the mathematical way for balancing the rotating system analytically.

Keywords: mass imbalance, condition monitoring, vibration analysis, static and dynamic balance..

1. Introduction

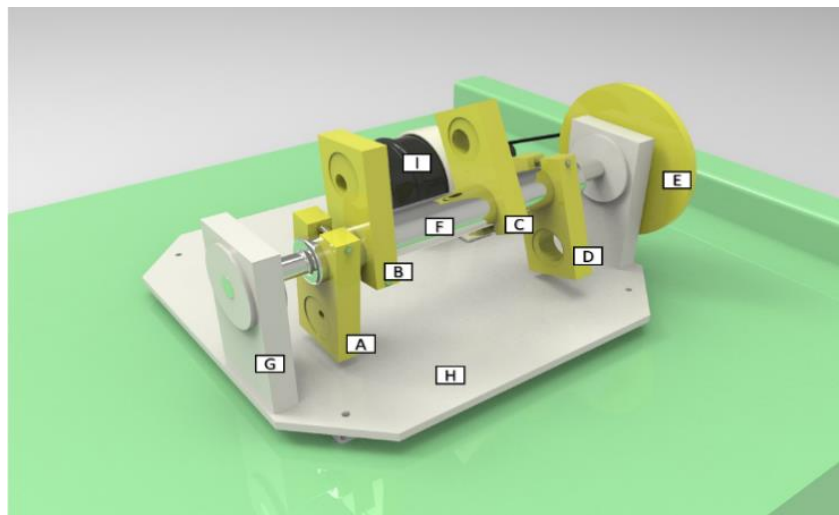
Vibration is a familiar signature for rotating machinery which is developed by mass imbalance and the mass imbalance comprises static or forced imbalance and dynamic or quasi-static imbalance. If a rotor is supported by bearings which carries heavy spot at the mid-point between them, the static imbalance is formed and can be identified by the weight distribution axes which is parallel to the rotational axes. On the contrary, dynamic balancing aggregates static and couple imbalance which forms when the weight distribution and rotational axes don't intersect at all and it's a common phenomenon in rotating machinery. When vibrational parameters in rotating machinery exceeds the satisfactory level, it may cause severe damage to the machinery. That's why condition monitoring of the components of the machinery is much important which is performed in a regular scheduling to protect the machines. In case of fault diagnosis of rotating machineries a number of methods [1-7] have been developed such as statistical analysis, principal components analysis, model based diagnosis, oil/debris analysis, vibration analysis, temperature monitoring, acoustic emission monitoring etc.. Vibration based condition monitoring is must popular and well accepted in plants to meet this requirement because the machine vibration response is sensitive to any small structural or process parameter change [8]. According to Farrar and Doebling, the most nature and successful application of vibration based damage detection technology has been in the monitoring of rotating machinery [9]. The apparatus comprises a sturdy base unit with four flexible mounts with a rotating shaft including four different masses at different angular and longitudinal positions at the shaft which is driven by an electric motor. Additionally, two vertical stands support the circular shaft along with a base supports the entire setup. Furthermore, the first three masses are fixed at a particular angular and longitudinal position, only 4th mass can be operated to minimize the high level of vibration generating in the apparatus due to mass imbalance.

A CSI 2140 machinery health analyzer has been used to measure the vibrational parameters of the apparatus at different angular positions of the 4th mass using static and dynamic balancing. This paper aims to focus on the effects of mass imbalance that causes heavy signature of vibration in addition to damages or failure of the rotating machineries. This minimization of the imbalance due to mass has been done by static and dynamic balancing procedure. It has been seen that when the apparatus is balanced at 338° angular position of the 4th mass, the amplitude displayed in the analyzer is minimum than other angular positions of the 4th mass.

2. Mathematical modelling and methodology

In static and dynamic balancing apparatus, an electric motor is used to power the test assembly in which the shaft is turned electrically for dynamic balancing. During dynamic balancing test, the assembly undergoes vibration which is allowed by the flexible mount in order to show mass imbalance. For static balancing, the shaft is kept static at any angular position which is done by removing the belt.

The electrical power given to the motor drives it which further drives the shaft by a pulley arrangement where a round belt connects both of the pulley. Four masses with different weight and angular and longitudinal positions are placed around the shaft. The shaft starts rotating in accordance with the rotation of the electrical motor which also causes rotation of the four different masses in anticlockwise. A signature of vibration occurs as a result of mass imbalance which is taken in the machinery analyzer in terms of amplitude where frequency is displayed within the abscissa. When steep vibration occurs due to the imbalance, the apparatus can be balanced by static and dynamic balancing by fixing the 4th mass considering its angular position. The schematic of the apparatus is given below in the following figure.



Annotations: A. 1st mass B. 2nd mass C. 3rd mass D.4th mass E. Large pulley F. Shaft
G. Vertical Stand H. Base I. Motor

Figure 1: Static and Dynamic Balancing Apparatus

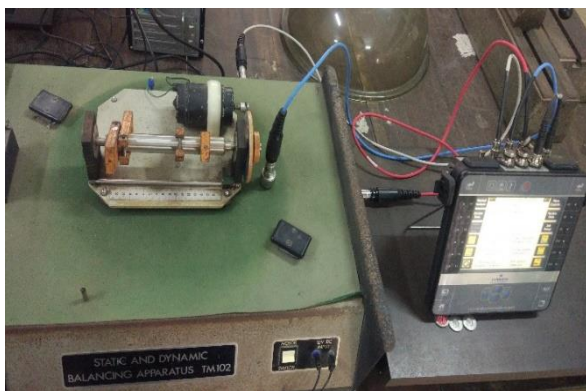


Figure 2: Static and dynamic balancing apparatus with Measurement of vibration at base.

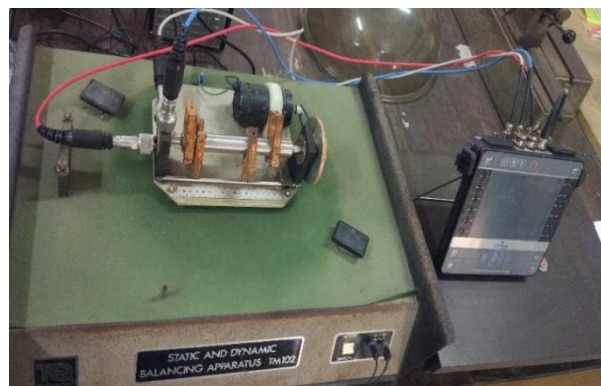


Figure 3: Static and dynamic balancing apparatus With measurement of vibration at vertical stand

The magnitude and direction of the 4th mass for static and dynamic balance have been obtained analytically.

Magnitude and direction for static balance:

The moment tending to turn the shaft due to out of balance are:

Table 1: Moments with direction of the masses

Mass	Moment	Direction
1	$w_1 r_1 \cos \alpha_1$	Clockwise
2	$w_2 r_2 \cos \alpha_2$	Clockwise
3	$w_3 r_3 \cos \alpha_3$	Clockwise
4	$w_4 r_4 \cos \alpha_4$	Clockwise

For static balance, it is known that,

$$w_1 r_1 \cos \alpha_1 = w_2 r_2 \cos \alpha_2 + w_3 r_3 \cos \alpha_3 + w_4 r_4 \cos \alpha_4 \dots\dots\dots (1)$$

$$w_1 r_1 \sin \alpha_1 = w_2 r_2 \sin \alpha_2 + w_3 r_3 \sin \alpha_3 + w_4 r_4 \sin \alpha_4 \dots\dots\dots (2)$$

Where, w_1, w_2, w_3, w_4 = Distributing masses in the shaft
 r_1, r_2, r_3, r_4 = Distance from the axes of the rotating shaft
 $\alpha_1, \alpha_2, \alpha_3, \alpha_4$ = angles of these mass with horizontal axes respectively

Magnitude and direction for dynamic balance:

All of the masses placed in the shaft are subjected to centrifugal forces when the shaft is rotating. There are two conditions which must be satisfied if the shaft is not to vibrate at the time of rotating at high speed. The conditions are:

- (a) Out of balance centrifugal forces trying to deflect the shaft must not be presented while rotating the shaft.
- (b) Out of balance moment or couple trying to twist the shaft must be avoided.

For no out of balance force, sum of horizontal components and sum of vertical components of centrifugal force must be zero. i.e.

$$\sum F_x = 0 \quad \text{and} \quad \sum F_y = 0$$

$$\Rightarrow \frac{w_1}{g} \omega^2 r_1 \cos \alpha_1 = \frac{w_2}{g} \omega^2 r_2 \cos \alpha_2 + \frac{w_3}{g} \omega^2 r_3 \cos \alpha_3 + \frac{w_4}{g} \omega^2 r_4 \cos \alpha_4$$

$$\Rightarrow w_1 r_1 \cos \alpha_1 = w_2 r_2 \cos \alpha_2 + w_3 r_3 \cos \alpha_3 + w_4 r_4 \cos \alpha_4$$

This is actually the same result obtained for static balance. Thus it can be said that if the shaft is statically balanced then it will also be dynamically balanced.

Table 2: Data for the statically and dynamically balanced Shaft

Mass no.	Angle(°), α	Distance (mm), r	Mass weight (gm), W
01	0	5	190
02	150	105	180
03	190	25	170
04	337.94 \approx 338	145	160

In order to determine the values of r_4 and α_4 , it can be written from equation (i),

$$190 \times 5 \cos 90^\circ = (180 \times 105 \cos 150^\circ) + (170 \times 25 \cos 190^\circ) + (160 \times r_4 \cos \alpha_4)$$

$$\Rightarrow r_4 \cos \alpha_4 = 134.4$$

Similarly from equation (ii),

$$\text{So, } \frac{r_4 \sin \alpha_4 = 54.45}{\frac{r_4 \cos \alpha_4 = 134.4}{r_4 \sin \alpha_4 = 54.45}}$$

$$\Rightarrow \alpha_4 = 337.94^\circ \quad \text{and} \quad r_4 = 145 \text{ mm}$$

3. Result and discussion

This experiment has been aimed to achieve a stable system depending on the ISO standard from an unstable system. Due to mass imbalance in the static and dynamic balancing apparatus, vibration data is recorded which signifies the different levels of vibration at the sturdy bas and the vertical stands which supports the shaft for different angular position of the 4th mass. Here, the vibrational data is obtained by the use of CSI 2140 machinery

health analyzer which consists of three accelerometer which placed at right angle to each other. For making possible of dynamic balancing of the apparatus, the angular position of the 4th mass has been calculated by analytical method. After calculating the angle and longitudinal direction of the 4th mass from the left vertical stand which supports the steel shaft, the vibration data in terms of amplitude has been taken from the analyzer by performing spectrum analysis. Now, whether the angular position of the 4th mass is ok not, can be proved experimentally by taking vibrational data for other angular position of the 4th mass. Here the angle is 338° and longitudinal distance is 145 mm of the 4th mass for perfectly balanced position of the apparatus. And vibrational data has been taken for angle of 333°, 338°, 343° of the 4th mass rotating at anticlockwise direction and vibrational data has been measured. A comparison of sensitiveness of the apparatus to vibration of different angular position which is measured at the base and at the vertical stands has been showed below presenting the spectrum analysis and a bar chart.

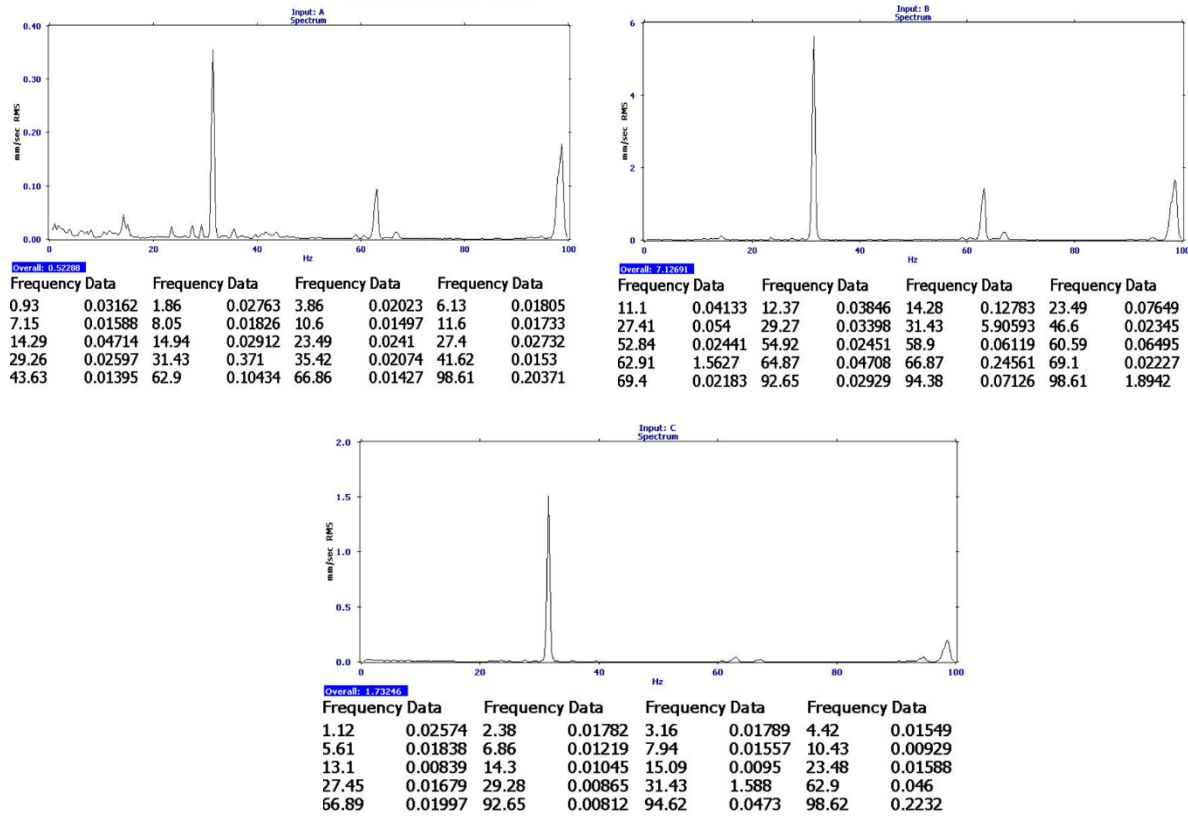
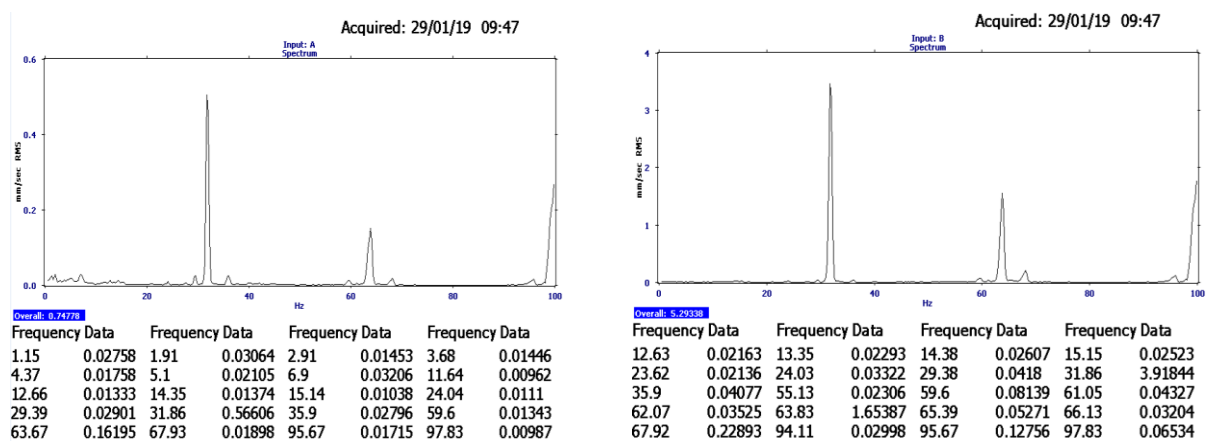


Figure 4: Frequency and amplitude for Input A, B, C for Angle 328° considering the base at unbalanced condition



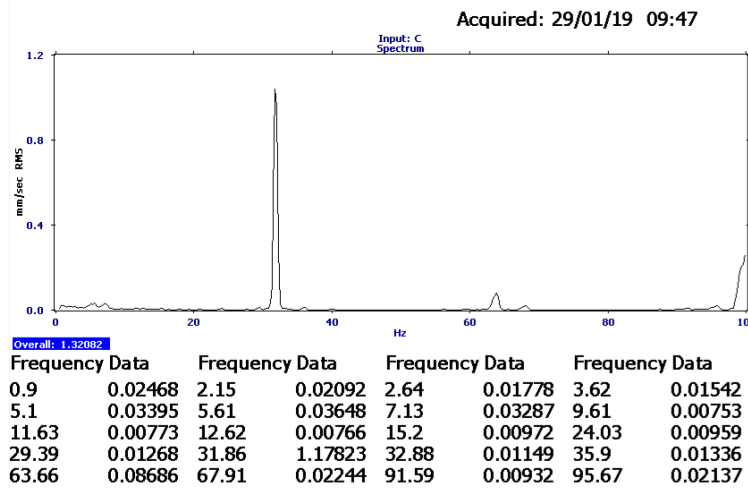


Figure 5: Frequency and amplitude for Input A, B, C for Angle 338° considering the base at balanced condition

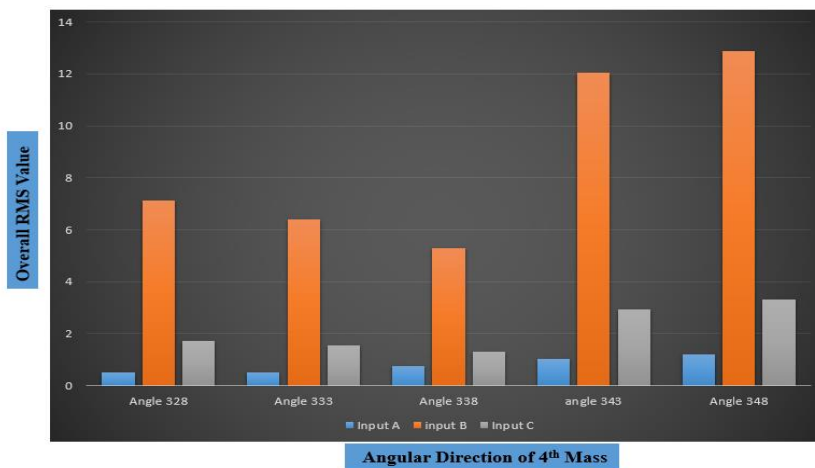


Figure 6: Comparative Illustration of the Overall RMS Value for Different Angular Position of the 4th Mass When Considering Vibration at Base

It can be seen from the bar chart that the overall RMS values has been reduced at base of the apparatus at angle of 338° as this angle is the perfect position for the 4th mass for static and dynamic balancing which has been measured analytically.

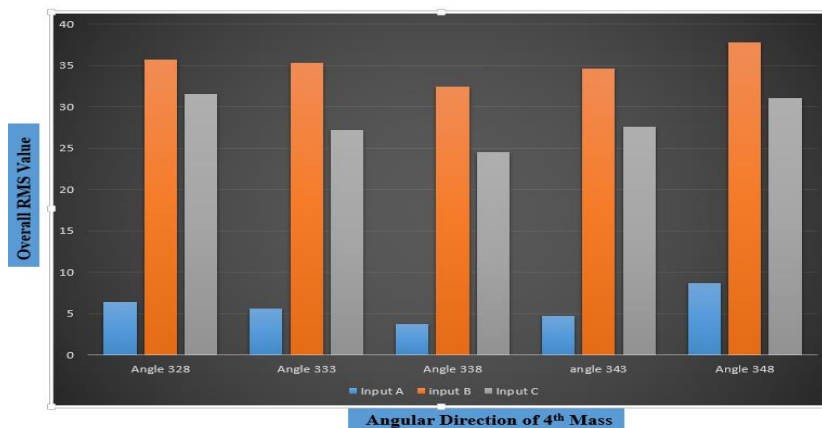


Figure 7: Comparative Illustration of the Overall RMS Value for Different Angular Position of the 4th Mass When Considering Vibration at Vertical Stand

It can be seen from the bar chart that the overall RMS values has been reduced at vertical stand of the apparatus at angle of 338° as this angle is the perfect position for the 4th mass for static and dynamic balancing which has been measured analytically.

4. Conclusion

The amount of vibration imposed in the static and dynamic balancing apparatus due to mass imbalance has been observed in this paper. Furthermore, the minimization of the vibration which is measured by using machinery health analyzer has been completed by static and dynamic balancing procedure. In case of rotation of a single mass with multiple masses in different planes, vibration often occurs when weight distribution axes and rotational axes don't coincide each other. Then the characteristics vibration undertaken generated a spectral plot which indicated that mass imbalance was mostly one of the causes for this signature. In accordance with, the angular and longitudinal position of the 4th mass has been calculated analytically which was 338° and 145 mm respectively in order to mitigate the additional vibrational generated by mass imbalance. Moreover, a comparison has also been shown in terms of vibration for different angular position of the 4th mass in this paper.

5. References

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